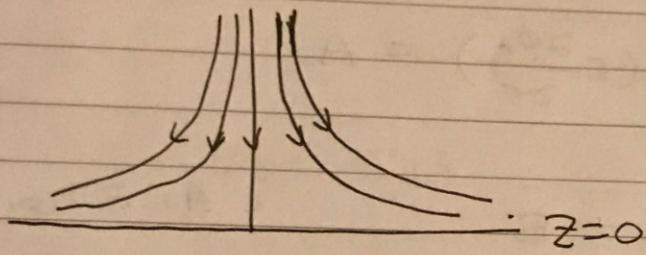


BI 2016

① irrotational flow  $\nabla \times \underline{u} = 0$   
 $\Rightarrow \underline{u} = \nabla \phi$

incompressible flow  $\nabla \cdot \underline{u} = 0$

$\therefore \nabla \cdot \nabla \phi = 0 \Rightarrow \underline{\underline{\nabla^2 \phi}} = 0$



Near the vicinity of  
the stagnation point

The surface is locally  
flat.

$\therefore$  object is impenetrable  $\Rightarrow$

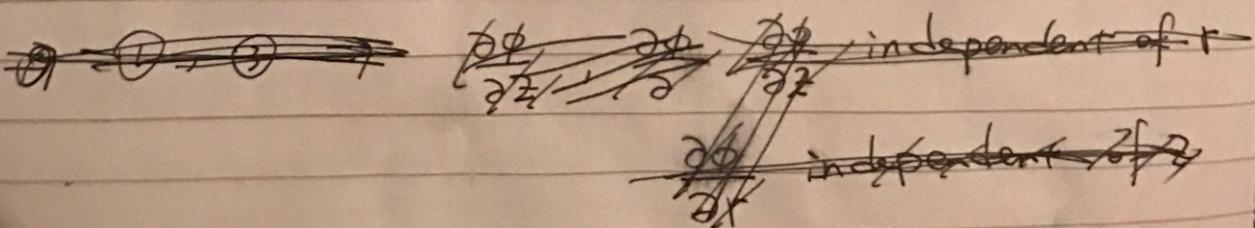
$\therefore u_z = 0 \text{ at } z = 0 \Rightarrow \frac{\partial \phi}{\partial z} \Big|_{z=0} = 0 \quad (1)$   
(for all  $r$ )

The  $x, y$  directions are symmetric, so we switch to cylindrical polar coordinates.

$\underline{u} = (u_r, u_\theta, u_z) \text{ where } u_\theta = 0$

$\therefore \nabla^2 \phi = 0 \quad \therefore \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial \phi}{\partial r} \right) + \frac{\partial^2 \phi}{\partial z^2} = 0 \quad (2)$

Also by symmetry  $\frac{\partial \phi}{\partial r} \Big|_{r=0} = 0 \quad (3)$   
(for all  $z$ )



The the trial solution

$$\phi(r, z) = \phi_r(r) + \phi_z(z)$$

$$\therefore \textcircled{2} \Rightarrow \frac{1}{r} \underbrace{\frac{\partial}{\partial r} \left( r \frac{\partial \phi_r}{\partial r} \right)}_{\text{a function only of } r} + \underbrace{\frac{\partial^2 \phi_z}{\partial z^2}}_{\text{a function only of } z} = 0$$

$$\therefore \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial \phi_r}{\partial r} \right) = A$$

$$\frac{\partial^2 \phi_z}{\partial z^2} = B \quad (A, B \text{ constants})$$

$$\Rightarrow \frac{\partial}{\partial r} \left( r \frac{\partial \phi_r}{\partial r} \right) = rA \Rightarrow r \frac{\partial \phi_r}{\partial r} = \frac{A}{2} r^2 + C$$

$$\Rightarrow \frac{\partial \phi_r}{\partial r} = \frac{A}{2} r + \frac{C}{r}$$

$\therefore$  at  $r=0$ ,  $\frac{\partial \phi_r}{\partial r}$  is not going to  $\infty$

$$\therefore C=0 \quad \therefore \frac{\partial \phi_r}{\partial r} = \cancel{\frac{A}{2} r} \quad (\cancel{\text{constant}})$$

$$\therefore \phi_r = \frac{A}{4} r^2 + D \quad (\text{any additive constant can be set to 0} \quad \therefore D=0)$$

$$\Rightarrow \phi_r = \cancel{\frac{A}{4}} Ar^2 \quad (\text{absorb } \frac{1}{4} \text{ into } A)$$

$$\frac{\partial^2 \phi_z}{\partial z^2} = B \rightarrow \frac{\partial \phi_z}{\partial z} = Bz + E$$

$$\therefore \text{At } z=0 \quad \frac{\partial \phi_z}{\partial z} = \frac{\partial \phi}{\partial z} = 0 \quad \therefore E=0$$

$$\therefore \frac{\partial \phi_z}{\partial z} = Bz \quad \therefore \phi_z = \frac{B}{2}z^2 + F$$

absorb  $\frac{1}{2}$   
into B

$\hookrightarrow$  can be  
set to 0

$$\therefore \phi_z = Bz^2$$

$$\therefore \text{we have } \phi(r, z) = Ar^2 + Bz^2$$

$$\text{Then } \nabla^2 \phi(r, z) = 0$$

$$\therefore \cancel{\frac{1}{r} \frac{\partial}{\partial r}} \left( r \cdot 2Ar \right) + 2B = 0$$

$$\therefore 4A + 2B = 0$$

~~$\therefore u_z < 0$~~   ~~$B < 0$~~  for  $z > 0$

$$\therefore B < 0 \quad \therefore \text{let } \cancel{2B} = -B \quad B = -2w$$

$$\text{then } A = w, B = -2w$$

$$\therefore \phi(r, z) = w(r^2 - 2z^2) \quad \because r^2 = x^2 + y^2$$

$$\therefore \phi(x, y, z) = w(x^2 + y^2 - 2z^2)$$

$w > 0$

→ This solution is unique up to an additional constant due to the uniqueness theorem of first order derivative boundary conditions

The streamlines:

$$\frac{dx}{u_x} = \frac{dy}{u_y} = \frac{dz}{u_z}$$

$$u = \nabla \phi = 2w(x, y, -2z)$$

$$\therefore \frac{dx}{x} = \frac{dy}{y} = -\frac{dz}{2z} \quad \ln x = \ln z + f(y)$$

integrate  $\ln x = \ln y + C_1 = -\frac{1}{2} \ln z + C_2$

$$\therefore \ln \frac{y}{x} = \text{const} \quad y = \text{const} \times x$$

$$\ln z = -2 \ln x + \text{const}$$

$$\therefore \ln(zx^2) = \text{const} \quad z = \frac{\text{const}}{x^2}$$

$$\therefore \text{streamline is } y = kx = \frac{m}{\sqrt{z}} \quad (k, m \text{ are constants})$$

$$\therefore z = \frac{c_1(y)}{x^2} + f(y), \quad z = \frac{c_2(x)}{y^2} + g(x) \Rightarrow z = \frac{c}{x^2 + y^2}$$

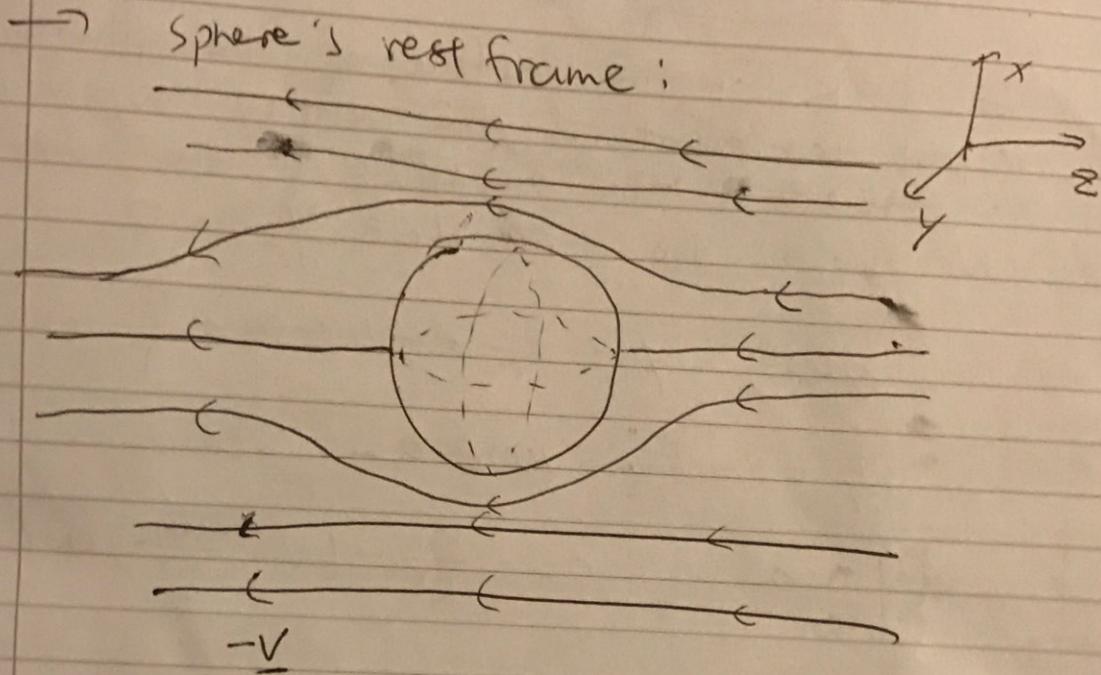
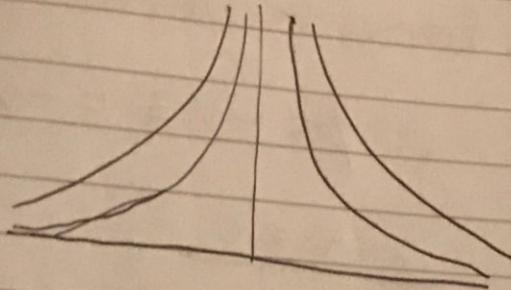
$$\therefore x^2 = \text{const}$$

$$y^2 = \text{const}$$

$$x^2 + y^2 = \text{const}$$

$$\therefore z = \frac{c}{x^2 + y^2}$$

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tional  
theore



In the rest frame of the sphere, the fluid moves with a constant velocity  $-V$  ( $V$  in negative  $\hat{z}$  direction), while the sphere is at rest.

$$\text{Assume } \phi(r, \theta) = A_0 + \frac{B_0}{r} + (A_1 r + \frac{B_1}{r^2}) \cos \theta$$

is the velocity potential. ~~The system has azimuthal symmetry. So only  $r, \theta$  are relevant.~~

• This form of  $\phi$  automatically solves  $D^2\phi = 0$

We now only need to worry about the boundary conditions.

→ At large  $r$  away from the sphere,

$$\underline{u} = (0, 0, -v) \quad \therefore \phi = -vz = -vr\cos\theta$$

$$\therefore \underline{A}_1 = -v \quad , \quad \underline{A}_0 = 0$$

At  $r=R$  on the surface of the sphere, the normal component of the velocity with respect to  ~~$\underline{u}(r)$~~   $= \underline{u}$  the surface of the sphere is 0 (No slip) i.e.  ~~$u_r = \frac{\partial \phi}{\partial r} = 0$~~

$$\text{i.e. } \cancel{\frac{\partial \phi}{\partial r}} \quad \therefore \phi = \frac{B_0}{r} + -vr\cos\theta + \frac{B_1}{r^2}\cos\theta$$

$$\therefore \frac{\partial \phi}{\partial r} = -\frac{B_0}{r^2} - v\cos\theta + -\frac{2B_1}{r^3}\cos\theta$$

$$\therefore \left. \frac{\partial \phi}{\partial r} \right|_{r=R} = 0 \quad \therefore 0 = -\frac{B_0}{R^2} - \left( v + \frac{2B_1}{R^3} \right) \cos\theta$$

$$\therefore \text{We need } \underline{B}_0 = 0 \quad \text{and} \quad \underline{B}_1 = -\frac{VR^3}{2}$$

$$\therefore \phi(r, \theta) = -v\cos\theta \left( r + \frac{R^3}{2r^2} \right)$$

$$\text{velocity } \underline{u}(r) = \nabla \phi = u_r \hat{r} + u_\theta \hat{\theta}$$

$$u_r = \frac{\partial \phi}{\partial r} = -v\cos\theta \left( 1 - \frac{R^3}{r^3} \right)$$

$$u_\theta = \frac{1}{r} \frac{\partial \phi}{\partial \theta} = v\sin\theta \left( 1 + \frac{R^3}{2r^3} \right)$$

The stagnation points are  $(u_r, u_\theta) = (0, 0)$

$$\Rightarrow A(r, \theta) = \underline{\underline{(R, 0)}}$$

$$B(r, \theta) = (R, \pi)$$

$$\text{velocity potential } \phi = -V \cos \theta \left( r + \frac{R^3}{2r^2} \right)$$

→ Near the stagnation point A,  ~~$\rho \neq 0$~~  let  $\rho^2 = x^2 + y^2$   
so that  $r^2 = \rho^2 + z^2$ ,  $z = r \cos \theta$

$$\therefore \phi = -Vz \left( 1 + \frac{1}{2} R^3 (\rho^2 + z^2)^{-3/2} \right)$$

Near A,  $z \approx R$   $\rho \ll R$   $\therefore$  let  $z = R + \delta$

$$\phi = -V(R + \delta) \left[ 1 + \frac{1}{2} R^3 \left( \rho^2 + (R + \delta)^2 \right)^{-3/2} \right]$$

$$= -V(R + \delta) \left[ 1 + \frac{1}{2} R^3 \left( (\rho^2 + \delta^2) + 2\delta R + R^2 \right)^{-3/2} \right]$$

$$= -V(R + \delta) \left[ 1 + \frac{1}{2} \left( 1 + \frac{2\delta}{R} + \frac{\delta^2 + \rho^2}{R^2} \right)^{-3/2} \right]$$

$$= -RV \left( \frac{3}{2} + \frac{3\delta^2}{2R^2} \right)$$

\* Taylor expansion for  $(1+x)^{-3/2}$  is

$$\text{if } \theta=0 \\ \text{cos } \theta \approx 1 - \frac{\theta^2}{2} \\ \therefore \phi \approx -V \left( 1 - \frac{\delta^2}{2R^2} \right)$$

$$(1+x)^{-3/2} \approx 1 - \frac{3}{2}x + \frac{15}{8}x^2 - \dots$$

$$\therefore -RV \left( \frac{3}{2} + \frac{3\delta^2}{2R^2} \right) \left[ 1 + \left( \frac{2\delta}{R} + \frac{\delta^2 + \rho^2}{R^2} \right) \right]^{-3/2} \approx 1 - \frac{3}{2} \left( \frac{2\delta}{R} + \frac{\delta^2 + \rho^2}{R^2} \right)$$

$$= -\frac{3}{2} RV + \frac{3V}{R} \left( (R\theta)^2 - 2\delta^2 \right) + \left( \frac{2\delta}{R} + \frac{\delta^2 + \rho^2}{R^2} \right) \times \frac{15}{8}$$

$$= 1 - \frac{3\delta}{R} - \frac{3\delta^2}{2R^2} - \frac{3\rho^2}{2R^2} + \frac{15}{2} \frac{\delta^2}{R^2} + O(\frac{\delta}{R})^3$$

$$\approx 1 - \frac{3\delta}{R} + \frac{6\delta^2}{R^2} - \frac{3\rho^2}{2R^2}$$

$$\begin{aligned}
 \therefore \phi &\approx -V(\delta+R) \left[ 1 + \frac{1}{2} - \frac{3\delta}{2R} + \frac{3\delta^2}{R^2} - \frac{3\rho^2}{4R^2} \right] \\
 &= -\cancel{\frac{V}{2}} - \frac{3V\delta}{2} + \frac{3V\delta^2}{2R} - \frac{3VR}{2} + \cancel{\frac{3V\delta}{2}} \\
 &\quad - \frac{3V\delta^2}{R} + \frac{3V\rho^2}{4R} + O(\delta^3) \\
 &\approx -\frac{3VR}{2} + \cancel{\frac{3V}{4R}} \cancel{(\rho^2 - 2\delta^2)}
 \end{aligned}$$

$\therefore \phi$  near A is (ignore constant  $-\frac{3VR}{2}$ )

$$\begin{aligned}
 \phi_A &= \frac{3V}{4R} (\rho^2 - 2\delta^2) \\
 &= \frac{3V}{4R} (x^2 + y^2 - 2(z-R)^2)
 \end{aligned}$$

as expected.

→ Similar near point B

$$\begin{aligned}
 \phi &= -Vr \cos\theta \left( 1 + \frac{R^3}{2r^3} \right) \quad \text{let } \rho^2 = x^2 + y^2, r^2 = \rho^2 + z^2 \\
 \text{Near B } z < 0, z \approx -R \quad &\text{let } \delta = R - z \\
 &\text{let } \delta = -R - z \quad \therefore z = R + \delta \quad \therefore z = -R - \delta \\
 &\therefore z = -R - \delta = -(R + \delta)
 \end{aligned}$$

$\therefore$  replace R by  $-R$ ,  $\delta$  by  $-\delta$  in  $\phi_A$  we get

$$\underline{\phi_B = -\frac{3V}{4R} (x^2 + y^2 - 2(z+R)^2)} \quad \text{as expected}$$

~~we~~  
The Bernoulli equation  $\frac{U^2}{2} + \frac{P}{\rho} = \text{const}$

$$U_r = -V \cos \theta \left(1 - \frac{R^3}{r^3}\right)$$

$$U_\theta = V \sin \theta \left(1 - \frac{R^3}{2r^3}\right)$$

At stagnation point  $U=0 \therefore P=P_0$

$$\therefore \text{const} = \frac{P_0}{\rho} \quad \therefore \frac{U^2}{2} + \frac{P}{\rho} = \frac{P_0}{\rho}$$

$$\therefore P = P_0 - \frac{1}{2} \rho U^2$$

~~$$U^2 = U_r^2 + U_\theta^2 = -V^2 \cos^2 \theta \left(1 - \frac{R^3}{r^3}\right)$$~~

on the surface of the sphere:  ~~$U_r = 0$~~   $U_r = 0$

~~$$U = U_\theta \hat{\theta}$$~~ 
$$\therefore U^2 = U_\theta^2(R)$$

~~$$U_\theta = V \sin \theta$$~~ 
$$U_\theta(R) = V \sin \theta \left(1 - \frac{R^3}{2R^3}\right) = \frac{1}{2} V \sin \theta$$

$$\therefore P = P_0 - \frac{1}{2} \rho \left(\frac{1}{2} V \sin \theta\right)^2$$

$$\rightarrow P = P_0 - \underbrace{\frac{1}{8} \rho V^2 \sin^2 \theta}_{}$$

(2)

Navier Stokes equation is

$$\frac{\partial \underline{u}}{\partial t} + (\underline{u} \cdot \nabla) \underline{u} + \frac{1}{\rho} \nabla p + g \underline{k} = \nu \nabla^2 \underline{u}$$

inertial term

viscous term

For slow viscous flow, Reynold number is small.  
The inertial term is negligible compare to the viscous term.

So ignore the inertial term

$$\frac{1}{\rho} \nabla p + g \underline{k} = \nu \nabla^2 \underline{u} \rightarrow \text{viscous term.}$$

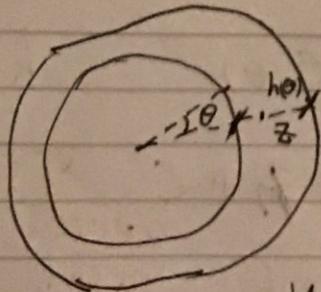
pressure term

gravity term

incompressibility requires

$$\nabla \cdot \underline{u} = 0$$

~~Reynolds~~ criteria : slow velocity  
small length scale.  
incompressible flow  
high viscosity.



Under lubrication approximation,

$$\nabla^2 \underline{u} \approx \frac{\partial^2 \underline{u}}{\partial z^2} \quad \text{for } \underline{u} = u_0 \\ = u(z, \theta)$$

We ignore the pressure gradient  $\nabla p$  since its effect is small compare to gravity

$\frac{\partial u}{\partial z} \sim \frac{U}{h}$   
 $\frac{\partial u}{\partial z^2} \sim \frac{U}{h^2}$   
 $\frac{\partial u}{\partial z} \sim \frac{U}{R}$   
 $\frac{\partial u}{\partial z^2} \sim \frac{U}{R^2}$   
 $\therefore \nabla^2 u \sim \frac{U^2}{R^2}$

(The exact explanation to this, see H.K. Moffatt, "Behaviours of a viscous film on the outer surface of a rotating cylinder").

So the Stokes equation in  $\theta$  direction is

$$g \hat{k} \cdot \hat{\theta} = \nu \cancel{\frac{\partial^2 u}{\partial z^2}} \cancel{v \nabla^2 u} = \underline{\underline{u(\theta, z) / z = 0}}$$

$$g \hat{k} \cdot \hat{\theta} = \nu (\nabla^2 u) \cdot \hat{\theta} = \nu \frac{\partial^2 u}{\partial z^2} \quad \frac{\partial u}{\partial z} \Big|_{z=h} = 0$$

Variable  $u$  is  
sinusoidal  
 $\therefore \underline{\underline{u(\theta, z) =}}$

$$\therefore \underline{\underline{u(\theta, z) = g \cos \theta}}$$

$\frac{\partial u}{\partial x} + \frac{\partial u}{\partial y} + \frac{\partial u}{\partial z} = 0$  Boundary conditions for  $u(\theta, z)$

$$\text{No slip at } z=0 \Rightarrow \underline{\underline{u(\theta, 0) = U}}$$

No shear stress at  $z=h$

$$\Rightarrow \nu \frac{\partial u}{\partial z} \Big|_{z=h} = 0 \quad \therefore \frac{\partial u}{\partial z} \Big|_{z=h} = 0$$

$$\therefore \frac{\partial^2 u}{\partial z^2} = \frac{g}{\nu} \cos \theta$$

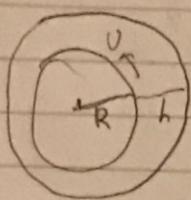
$$\therefore \frac{\partial u}{\partial z} = \frac{g}{\nu} \cos \theta z + C(\theta)$$

$$\text{At } z=h \quad 0 = \frac{g}{\nu} \cos \theta h + C \quad \frac{\nabla p}{\rho \nu D^2} \quad \underline{\underline{p = p_0}}$$

$$\therefore C = -\frac{g}{\nu} \cos \theta h \quad \frac{\rho \nabla p D^2}{h^2 (C.R.)}$$

$$\therefore \frac{\partial u}{\partial z} = \frac{g}{\nu} \cos \theta (z - h) \quad \frac{\rho \nabla p D}{h^2}$$

## Details of lubrication approximation



( $R \gg h$ )

$$\frac{1}{\rho} \nabla P + g \hat{k} = \nu \nabla^2 \underline{u}$$

$$z \text{ equation: } \frac{1}{\rho} \frac{\partial P}{\partial z} - g \sin \theta = u (\nabla^2 \underline{u})_z = \nu \left[ \nabla^2 u_z - \frac{(u_z)_z - \frac{1}{2} \frac{\partial u_z}{\partial \theta}}{(R+z)^2 (R+z)^2 \partial \theta} \right]$$

$$\cancel{\frac{\partial u_z}{\partial z} = \frac{u_z}{h}} \quad \frac{\partial^2 u_z}{\partial z^2} = \cancel{\frac{u_z}{h^2}} \quad \sim 0 \quad \sim 0 \quad \sim \frac{u_z}{R^2} \sim 0$$

$$\begin{aligned} \cancel{\nabla^2 u_\theta} &= \frac{1}{R+z} \frac{\partial}{\partial z} \left( (R+z) \frac{\partial u_\theta}{\partial z} \right) + \frac{1}{(R+z)^2} \frac{\partial^2 u_\theta}{\partial \theta^2} \\ &= \underbrace{\frac{1}{R+z} \frac{\partial^2 u_\theta}{\partial z^2}}_{\sim \frac{u_\theta}{h^2}} + \underbrace{\frac{1}{R+z} \frac{\partial u_\theta}{\partial z}}_{\sim \frac{u_\theta}{hR}} + \underbrace{\frac{1}{(R+z)^2} \frac{\partial^2 u_\theta}{\partial \theta^2}}_{\sim \frac{u_\theta}{R^2}} \\ &\checkmark \quad \times \quad \times \\ &\approx \frac{\partial^2 u_\theta}{\partial z^2} \end{aligned}$$

$$\nabla \cdot \underline{u} = 0 \Rightarrow \frac{1}{R+z} \frac{\partial}{\partial z} ((R+z) u_z) + \frac{1}{R+z} \frac{\partial u_\theta}{\partial \theta} = 0$$

$$\therefore \underbrace{\frac{\partial u_z}{\partial z}}_{\frac{u_z}{h}} + \underbrace{\frac{1}{R+z} u_z}_{\frac{u_z}{R}} + \underbrace{\frac{1}{R+z} \frac{\partial u_\theta}{\partial \theta}}_{\frac{u_\theta}{R}} = 0$$

$$\Rightarrow \cancel{u_z} \sim \frac{h}{R} u_\theta \approx 0 \quad (\because \ll u_\theta)$$

$$\therefore \nabla^2 u_z \approx 0 \quad \Rightarrow \underbrace{\frac{1}{\rho} \frac{\partial P}{\partial z} - g \sin \theta}_{\rho \approx \rho g h} = 0$$

$\theta$  equation

$$\therefore \underline{P \sim \rho g h}$$

$$\frac{1}{\rho} \frac{1}{R+z} \frac{\partial P}{\partial \theta} + g \cos \theta = \nu \nabla^2 u_\theta$$

$$= \nu \frac{\partial^2 u_\theta}{\partial z^2}$$

$$\Rightarrow \underbrace{g \cos \theta}_{\sim \frac{P}{\rho R}} = \nu \frac{\partial^2 u_\theta}{\partial z^2}$$

$$\sim \frac{P}{\rho R} \sim \frac{\rho g h}{\rho R} \sim \frac{h}{R} g \ll g$$

X

$$U = \frac{g}{v} + \underline{\underline{\left(\frac{z^2}{2}\right)}}$$

$$U = \frac{g}{v} \cos\theta \left( \frac{z^2}{2} - zh \right) + D(\theta).$$

At  $z=0$ ,  $\cancel{D(\theta)} \quad U = U$

$$\therefore U = D(\theta) \quad \therefore \quad U = U + \underline{\underline{\left( \frac{z^2}{2} - zh \right) \frac{g}{v} \cos\theta}}$$

$$Q = \int_0^h U dz = \int_0^h \left[ U + \left( \frac{z^2}{2} - zh \right) \frac{g}{v} \cos\theta \right] dz$$

$$= \cancel{U} \left[ U z + \left( \frac{z^3}{6} - \frac{z^2 h}{2} \right) \frac{g}{v} \cos\theta \right] \Big|_0^h$$

$$= Uh + h^3 \left( \frac{1}{6} - \frac{1}{2} \right) \frac{g}{v} \cos\theta$$

$$= \underline{\underline{Uh - \frac{h^3}{3} \frac{g}{v} \cos\theta}}$$

$$\text{If } H = \frac{Uh}{Q} \text{ then } \frac{1}{H} = \frac{Q}{Uh} \quad . \quad h = \frac{QH}{U}$$

$$\therefore \frac{1}{H} = 1 - \frac{gh^2}{3UV} \cos\theta \quad \left( \alpha = \frac{g\alpha^2 H^2}{3UV^3} \right)$$

$$= 1 - \frac{g\alpha^2 H^2}{3UV^3} \cos\theta = 1 - H^2 \alpha \cos\theta$$

$$\cancel{+} \quad \therefore \cancel{\alpha^2} \Rightarrow 1 - \frac{1}{H} = H^2 \alpha \cos\theta$$

$$\therefore \underline{\underline{\frac{1}{H^2} - \frac{1}{H^3} = \alpha \cos\theta}}$$

→  $Q$  is constant because the conservation of mass around one revolution of the fluid motion and that the fluid is incompressible

~~Some amount of liquid is flux is the flux of fluid is the same for~~

So same amount of fluid has to flow through each cross-section of different  $\theta$  per unit time.

$$\therefore \frac{1}{H^2} - \frac{1}{H^3} = \alpha \cos \theta \quad \therefore \alpha \cos \theta H^3 - H + 1 = 0$$

Incompressible  
⇒ constant

$$\therefore H = 1 + \alpha \cos \theta H^3 \quad \therefore \alpha \ll 1$$

Since assume a  $H$  close to 1. then let  $H = 1 + x$   
 $(x \ll 1)$

$$\therefore H = 1 + \alpha \cos \theta \{ 1 + O(x) \}$$

$$\begin{aligned} &= 1 + \alpha \cos \theta + O(\alpha^2) + \\ &= 1 + \alpha \cos \theta + O(\alpha^2, x^2) \end{aligned}$$

$$\therefore H \approx 1 + \alpha \cos \theta$$

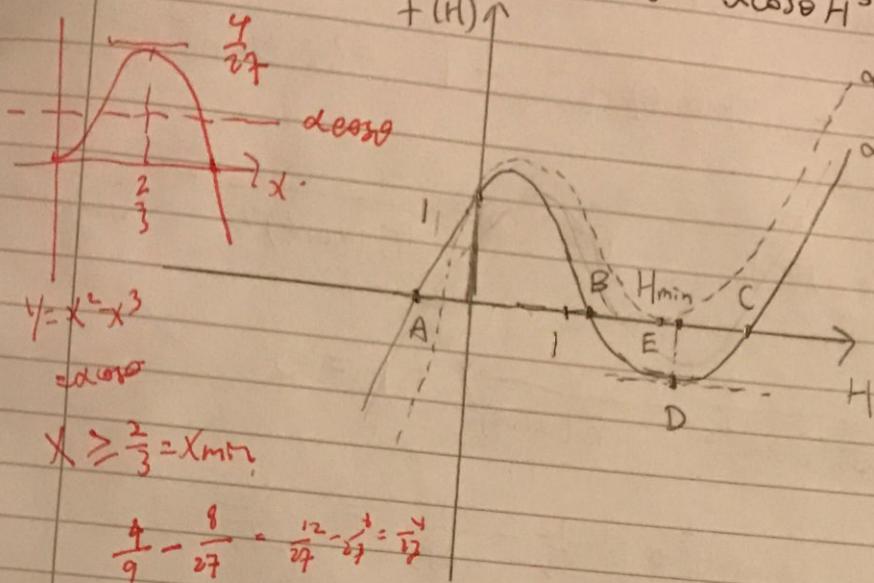
$$\therefore h(\theta) \approx \underline{\underline{\frac{Q}{J}(1 + \alpha \cos \theta)}}$$

Consider function

$$f(H) = \alpha \cos \theta H^3 - H + 1$$

$$\alpha = \frac{4}{27}$$

$\alpha \ll 1$



$$x \geq \frac{2}{3} = x_{\min}$$

$$\frac{4}{9} - \frac{8}{27} = \frac{12}{27} - \frac{8}{27} = \frac{4}{27}$$

Since  $f(0) = 1$ , one root of  $f$  must be negative.  
~~we call this~~ This is represented by point A.

Depend on the value of  $\alpha \cos \theta$ ,  $f$  can have 2 more roots (B and C) or one more root (E), or no more root.

If  $f$  has 2 more ~~roots~~ positive roots, then B is the perturbative solution we found earlier.

When  $\alpha \cos \theta$  is small, B is very close to 1. As  $\alpha \cos \theta$  increases, B and C get closer to each other. Eventually the local minimum of point D become positive and no more positive root does  $f(H)$  have.

The largest  $\alpha \cos \theta$  for  $f(H)$  to have positive root is when there is only one positive root E. The value of this root is  $H_{\min}$ .

then at point D,  $H = H_{\min}$

$$\Omega = \left. \frac{df}{dH} \right|_{H_{\min}} = 3(\alpha \cos \theta) H_{\min}^2 - 1 \Rightarrow H_{\min} = \frac{1}{\sqrt{3\alpha \cos \theta}}$$

$$\because f(H_{\min}) = 0 \quad \therefore \Omega = \alpha \cos \theta \cdot \frac{1}{3\sqrt{3}(\alpha \cos \theta)^{3/2}} - \frac{1}{\sqrt{3\alpha \cos \theta}} + 1$$

$$\therefore \frac{1}{3\sqrt{3}(\alpha \cos \theta)^{1/2}} - \frac{1}{\sqrt{3}(\alpha \cos \theta)^{1/2}} + 1 = 0$$

$\frac{\partial V}{\partial x} \approx \frac{\partial V}{\partial y}$

$$\therefore (\alpha \cos \theta)^{\frac{1}{2}} \approx \frac{1}{\sqrt{3}} - \frac{1}{3\sqrt{3}} = \frac{2}{3\sqrt{3}}$$

$$\therefore \alpha \cos \theta = \frac{4}{27} \text{ in that limiting case}$$

If ~~at~~ the upper limit of  $\alpha$ ,  $\alpha_{\max} > \frac{4}{27}$ , then in limiting case  $\cos \theta < 1$ . Then if we change  $\theta$  we can make  $\alpha \cos \theta > \frac{4}{27}$  and that the function  $f$  has no positive root.

So we must have  $\alpha_{\max} = \frac{4}{27}$

$$\rightarrow \underline{\alpha \leq \frac{4}{27}}$$

~~Solution for point C is not continuous~~  
if we reduce  $\alpha \cos \theta$  as  $\theta$  goes from 0 to  $\pi$  ( $\alpha \cos \theta$  goes from 0 to  $-\infty$ ,  $h(\theta)$  goes from  $\infty$  to 0) So this solution doesn't make sense.

The only solution that works is B.

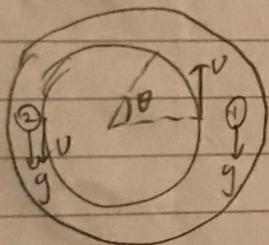
For B, larger  $\alpha \cos \theta$  gives larger  $h(\sigma)$

$\therefore \alpha \cos \theta$  is largest if  $\alpha \cos \theta = \frac{4}{27}$

$\therefore h_{\max} = \frac{Q}{\mu U} H_{\max}$ ,  $H_{\max}$  is the solution of

$$\frac{1}{H_{\max}^2} - \frac{1}{H_{\max}^3} = \frac{4}{27} \quad \therefore H_{\max} = \frac{3}{2}$$

$$\Rightarrow h_{\max} = \frac{\cancel{3Q}}{\cancel{2U}} \frac{3Q}{2U}$$



This phenomenon is due to the fact that the shear stress balances the gravitational force gravity.

At position ① gravity points down, the cylinder's velocity points up. The velocity gradient has to be negative along  $z$  & to counteract gravity. So velocity is small in ①  $h$  can be large to conserve  $Q$ .

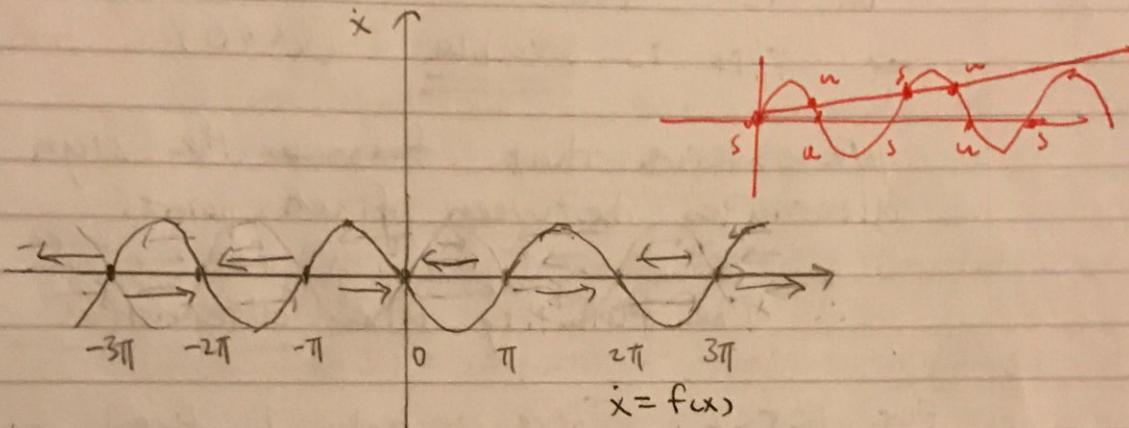
At position ② gravity points down, cylinder's velocity points down as well. The velocity gradient has to be positive in  $z$  to ~~counteract~~ counteract gravity. So velocity is large in ②.  $h$  should be small to conserve  $Q$ .

(3)

$$\dot{x} = rx - \sin x \quad r > 0 \quad f(x) = rx - \sin x$$

For  $r=0$   $\dot{x} = -\sin x$  fixed points  $\dot{x}=0$  for  $x=x^*$   
 $\Rightarrow -\sin x^* = 0$

$$\therefore \underline{x^* = n\pi \quad (n=0, \pm 1, \pm 2, \dots)}$$



stability : we calculate  $\frac{df}{dx} = \cancel{rx} - \cos x$

$$\therefore \left. \frac{df}{dx} \right|_{x^*} = -\cos(x^*) = -\cos(n\pi) = \underline{\underline{(-1)^{n+1}}}$$

$$\therefore \left. \frac{df}{dx} \right|_{x^*} \begin{cases} > 0 & \text{if } \underline{n \text{ is odd}} \Rightarrow \text{stable} \\ < 0 & \text{if } \underline{n \text{ is even}} \Rightarrow \text{unstable} \end{cases}$$

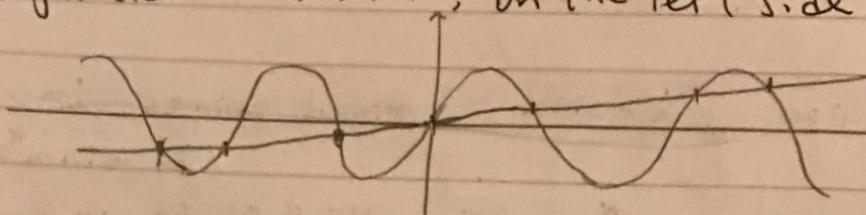
For  $0 < r \leq 2$

$$\dot{x} = f(x) = rx - \sin x \quad (\text{on real axis})$$

Fixed points  $\star f(x^*)=0 \therefore rx^* = \sin x^*$

When ~~0 < x < 0 < r < 1~~, the function  $g(x) = rx$  intersects with function  $h(x) = \sin x$  multiple times. There are more than 1 fixed points

For the ~~pink~~ fixed point  $x^* = 0$ , on the right side  $\sin x > rx$ , on the left side  $\sin x < rx$



$\therefore$  On RHS  $f(x) = rx - \sin x < 0$ , on LHS  $f(x) > 0$   
 $\Rightarrow$  This is stable ( $x^* = 0$ )

We observe that ~~fix~~ the sign of  $f(x)$  alternates between fixed points

$\therefore$  The stability also alternates

For  $1 < r < 2$ . There is only 1 fixed point  $x^* = 0$  and since  $f(x) > 0$  on RHS and  $< 0$  on LHS in this case, this is unstable

$\rightarrow$  For  $0 < r < 1$ :

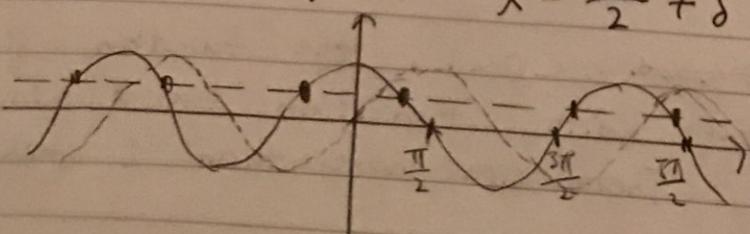
Bifurcation occurs ~~at~~ when  $g(x) = rx$  is tangent to  $h(x) = \sin x$

in this case:

$$g(x) = rx \quad g'(x) = r$$

$$\therefore \sin(x) = rx, \cos(x) = r$$

$$\therefore \cos(x) = r < 1 \quad \therefore x = \frac{n\pi}{2} + \delta$$



we see that for  $x > 0$ .  $\sin(x) = rx > 0$   
 since  $\cos(x) = r \ll 1$ ,  $x = \frac{n\pi}{2} - \delta$

we set  $x = \frac{n\pi}{2} - \delta \quad \because \cos(\frac{n\pi}{2}) = 0$   
 $(n = 1, 3, 5, 7, \dots)$

to focus on the tangent point  $x > 0$

For  $n = 3, 7, 11, \dots = 4m+3$

we see that  $\delta < 0$ , this corresponds to  
 $\sin(x) < 0$ , Not acceptable

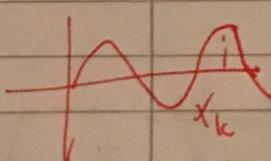
$\therefore \delta > 0, n = 1, 5, 9, \dots = 4m+1 \quad (m=1, 2, 3, \dots)$

$$\therefore \sin(\frac{4m+1}{2}\pi - \delta) = \sin(2m\pi + \frac{1}{2}\pi - \delta) = \sin(\frac{\pi}{2} - \delta) \\ = \cos(\delta) \approx 1$$

saddle node bifurcation

$$\cos(\frac{4m+1}{2}\pi - \delta) = \cos(\frac{4m\pi}{2} + \frac{1}{2}\pi - \delta) \approx \sin(\frac{1}{2}\pi - \delta) \\ \approx \cos(\frac{\pi}{2} - \delta) \approx \sin(\delta) \approx \delta$$

$\therefore$  we have  ~~$\sin(x) \approx 1$~~   $\sin(x) \approx 1$   $\cos(x) \approx \delta$



$$\therefore l = r(\frac{n\pi}{2} - \delta), \delta \approx r$$

$$\therefore l = r(\frac{n\pi}{2} - r) \text{ true}$$

$$x_k = 2\pi/c + \frac{1}{2}.$$

To first order in  $r$ , we have  $l = \frac{r n \pi}{2}$

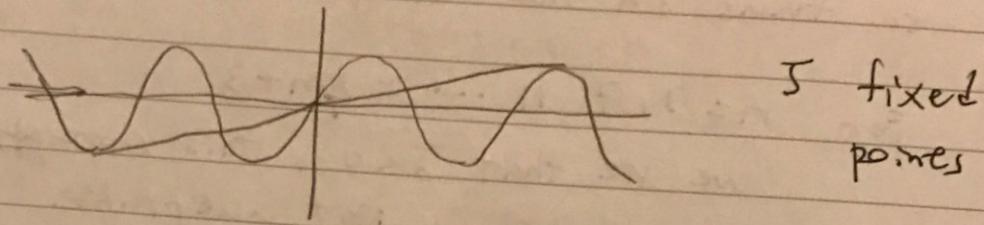
$$rx_k = l$$

$$r = \frac{l}{2\pi/c + \frac{1}{2}} \quad \therefore r = \frac{2}{n\pi} = \frac{2}{(4m+1)\pi} \quad (m=1, 2, 3, \dots)$$

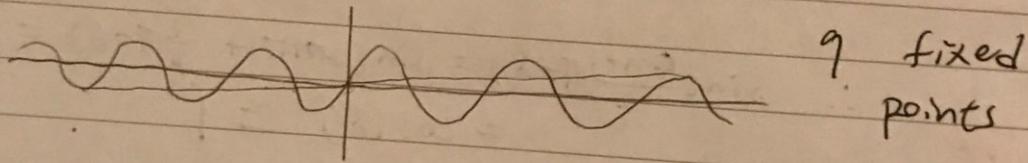
If  $m=0$ .  $r = \frac{2}{\pi}$  is an estimate to the tangent of first cusp, which should be  ~~$r=1$~~ .  $r=1$   
 This is poor. But for  $m \geq 1$ , since  $r$  is small

The approximation works well.

$\therefore r = \frac{2}{(4m+1)\pi}$  ( $m=1, 2, 3, \dots$ ), and  $r =$   
 are ~~fixed~~ Bifurcation points  
 $m=1$



$m=2$



$m=m$  ( $4m+1$ ) fixed points

If  $r \geq 1$ . only 1 fixed point  $x^* = 0$

$\therefore$  # of fixed points for  $0 < x \leq 2$  is

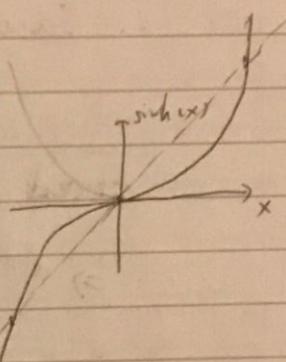
$$F(r) = \begin{cases} 4m+3 & \bullet \frac{2}{(4m+1)\pi} > r > \frac{2}{(4m+5)\pi} \\ 4m+1 & r = \frac{2}{(4m+1)\pi} \\ 3 & \bullet \frac{2}{5\pi} < r < 1 \\ 1 & 1 \leq r < 2 \end{cases}$$

If in imaginary axis  $x \rightarrow ix$

$$ix = irx - \sin(ix) = irx - \frac{e^{ix} - e^{-ix}}{2i}$$
$$= i(rx + \frac{1}{2}(e^{-x} - e^x))$$

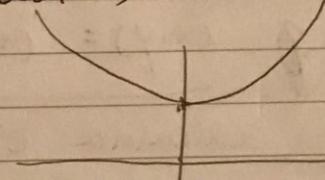
$$\therefore \dot{x} = rx + \frac{1}{2}(e^{-x} - e^x)$$

$$\therefore \dot{x} = rx - \sinh(x)$$



$$\therefore \frac{d}{dx} \sinh(x) = \cosh(x)$$

(and  $\cosh(x)$ )

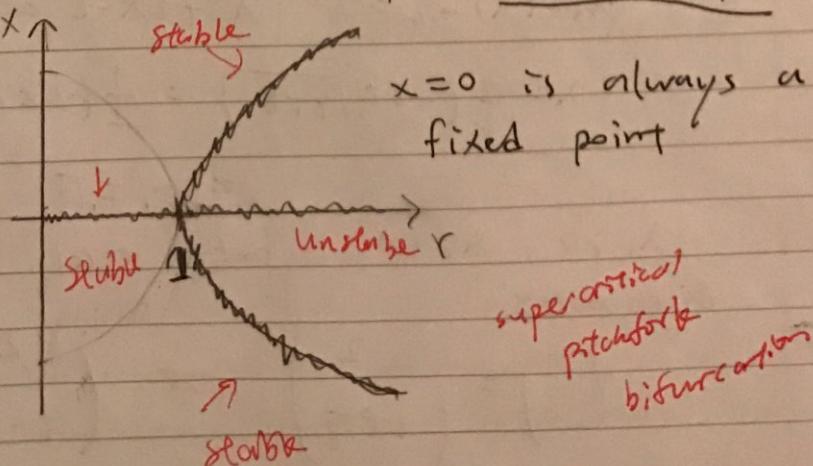


$\therefore$  the slope of  $\sinh(x)$  is always greater than 1

$\therefore$  If  $r \leq 1$ , then  $rx$  cannot intersect with  $\sinh(x)$  more than once

If  $r > 1$ ,  $rx$  intersects with  $\sinh(x)$  3 times.

Bifurcation occurs at  $r = 1$  only



## The system

$$\dot{x} = y^3 - y = f(x, y)$$

$$\dot{y} = x - y^2 = g(x, y)$$

∴ Jacobian  $J = \begin{pmatrix} \frac{\partial f}{\partial x} & \frac{\partial f}{\partial y} \\ \frac{\partial g}{\partial x} & \frac{\partial g}{\partial y} \end{pmatrix} = \begin{pmatrix} 0 & 3y^2 - 1 \\ 1 & -2y \end{pmatrix}$

fixed points  $x=0, y=0$

$$\Rightarrow \cancel{y \neq 0} \quad y(y+1)(y-1)=0 \quad , \cancel{x=y^2} \\ x = y^2$$

∴  $(x, y) = (0, 0), (1, 1), (1, -1)$

Classification: calculate eigenvalues  $\det(J - \lambda I) = 0$

$$(0, 0), J = \begin{pmatrix} 0 & -1 \\ 1 & 0 \end{pmatrix} \quad \therefore \lambda^2 + 1 = 0 \quad \lambda = \pm i \\ \text{centre}$$

$$(1, 1), J = \begin{pmatrix} 0 & 2 \\ 1 & -2 \end{pmatrix}$$

$$\lambda(2+\lambda) - 2 = 0 \quad \lambda^2 + 2\lambda - 2 = 0$$

$$\lambda = \frac{1}{2}(-2 \pm \sqrt{4+8}) = \frac{1}{2}(-2 \pm \sqrt{12}) \in \text{complex}$$

$\lambda_1 > 0, \lambda_2 < 0$        $= -1 \pm \sqrt{3}$   
 eigenvectors      both real       $\Leftrightarrow$  saddle node

$$\begin{pmatrix} 0 \\ 1 \end{pmatrix} = \begin{pmatrix} 2 \\ 1+\sqrt{3} \end{pmatrix} \quad \text{or} \quad \begin{pmatrix} 2 \\ 1-\sqrt{3} \end{pmatrix}$$

(1, -1)

$$J = \begin{pmatrix} 0 & 2 \\ 1 & 2 \end{pmatrix}$$

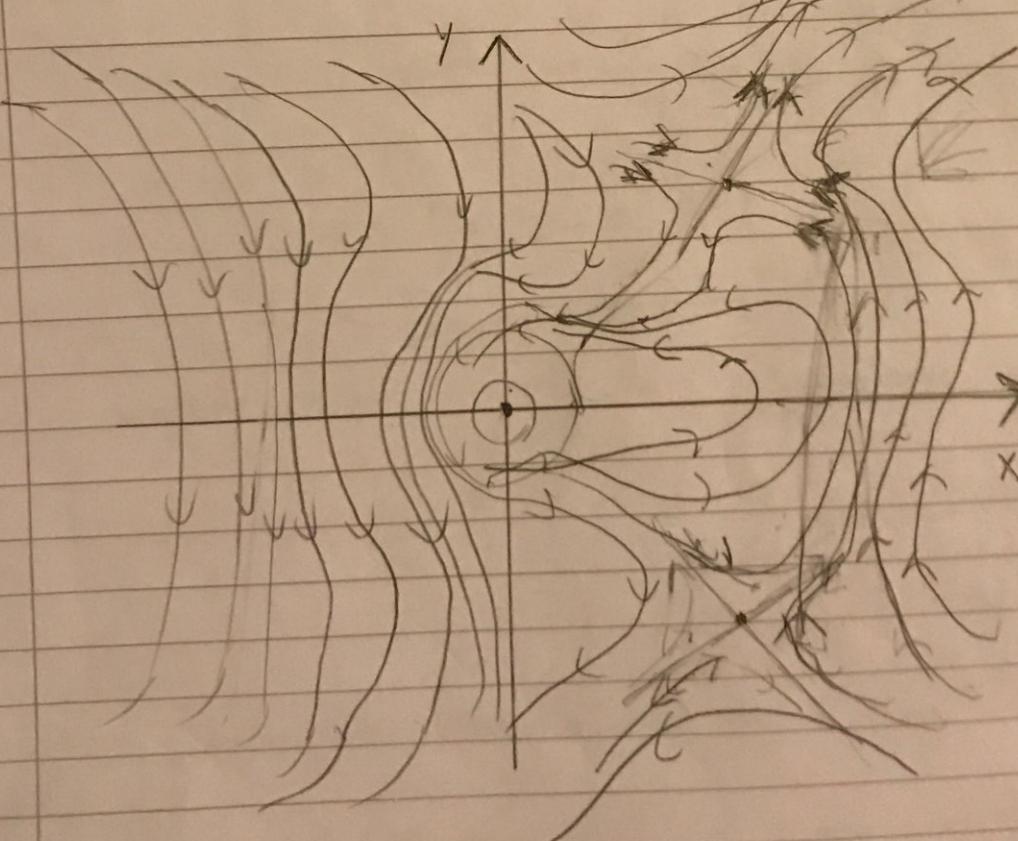
$$\bullet \lambda(\lambda-2)-2=0 \therefore \lambda^2-2\lambda-2=0$$

$$\lambda = \frac{1}{2}(2 \pm \sqrt{12}) = 1 \pm \sqrt{3}$$

$\lambda_1 > 0, \lambda_2 < 0 \therefore \underline{\text{saddle node}}$   
both real

eigenvectors ~~+/-~~  $\begin{pmatrix} a \\ b \end{pmatrix} (1 \pm \sqrt{3})a + 2b = 0$

$$\begin{pmatrix} a \\ b \end{pmatrix} = \begin{pmatrix} 2 \\ -(1+\sqrt{3}) \end{pmatrix} \text{ or } \begin{pmatrix} 2 \\ \sqrt{3}-1 \end{pmatrix}$$



$$4. \frac{dR}{dt} = k_R - \gamma_R R$$

$$\frac{dP}{dt} = k_P R - \cancel{\gamma_R} \gamma_P P$$

$$\therefore \frac{dR}{k_R - \gamma_R R} = dt.$$

$$\int_0^{R(t)} \frac{dR}{1 - \frac{\gamma_R}{k_R} R} = \int_0^t k_R dt$$

$$\therefore -\frac{k_R}{\gamma_R} \ln \left( 1 - \frac{\gamma_R}{k_R} R \right) = k_R t.$$

$$\therefore R = 1 - \frac{\gamma_R}{k_R} R = e^{-\gamma_R t}$$

$$\therefore R = \frac{k_R}{\gamma_R} (1 - e^{-\gamma_R t})$$

steady state  $\frac{dR}{dt} = 0, \frac{dP}{dt} = 0$

$$\therefore R = \frac{k_R}{\gamma_R}, P = \frac{k_P}{\gamma_P} R = \frac{k_P k_R}{\gamma_P \gamma_R}$$

single gene transcribed in 1 min

life time of RNA is 10 min  $\therefore \frac{1}{\gamma_R} = 10 \text{ min}$

$$\therefore R(1\text{ min}) = \frac{k_R}{\gamma_R} (1 - e^{-1/10})$$

$$= 0.095 \frac{k_R}{\gamma_R}$$

$$= \underline{0.095 k_R}$$

Now with the noise

$$\frac{dR}{dt} = k_R - \gamma_R R + \eta_R(t)$$

$$\text{let } R = \langle R \rangle + \delta R(t) \quad \text{with } \langle R \rangle = \frac{k_R}{\gamma_R}$$

$$\therefore \frac{d}{dt}(\langle R \rangle + \delta R) = k_R - \gamma_R \left( \frac{k_R}{\gamma_R} \right) - \gamma_R \delta R + \eta_R(t)$$

$$\therefore \dot{\delta R} = -\gamma_R \delta R + \eta_R(t)$$

Fourier transform

$$\delta R(t) = \int \frac{d\omega}{2\pi} e^{i\omega t} \tilde{\delta R}(\omega)$$

$$\therefore i\omega \tilde{\delta R}(\omega) = -\gamma_R \delta R(\omega) + \eta_R(\omega)$$

$$\delta R(\omega) = \frac{\eta_R(\omega)}{\gamma_R + i\omega}$$

$$\langle \eta_R(\omega) \eta_R^*(\omega') \rangle = \int dt \int dt' e^{i\omega t + i\omega' t'} \underbrace{\langle \eta_R(t) \eta_R^*(t') \rangle}_{g_R(t-t')}$$

$$= g_R \int dt e^{i(\omega+\omega')t}$$

$$= g_R \delta(\omega + \omega')$$

$$\langle \delta R(t) \delta R(t') \rangle = \iint \frac{dw}{2\pi} \frac{dw'}{2\pi} \underbrace{\langle \eta_R(w) \eta_R(w') \rangle}_{\delta(w+w')} \langle \tilde{\delta R}(w) \tilde{\delta R}(w') \rangle$$

$$= \iint \frac{dw}{2\pi} \frac{dw'}{2\pi} \frac{\langle \eta_R(w) \eta_R^*(w') \rangle}{(\gamma_R + iw)(\gamma_R + iw')} e^{iwt} e^{iwt'} \\ w = -w' \\ w^* = -w' \\ \therefore \langle \delta R(t) \delta R(t') \rangle = \int \frac{dw}{2\pi} \frac{\gamma_R}{\gamma_R^2 + w^2} = \underline{\underline{\frac{\gamma_R}{2\gamma_R}}}$$

$$\delta R \langle \delta P^2 \rangle = \langle P \rangle \left( 1 + \frac{k_p}{\gamma_R + \gamma_p} \right) \\ = \langle P \rangle \left( 1 + \frac{k_p/\gamma_R}{1 + \frac{\gamma_p}{\gamma_R}} \right) = \langle P \rangle \left( 1 + \frac{b}{1+\phi} \right) \\ b = \frac{k_p}{\gamma_R} \quad \phi = \frac{\gamma_p}{\gamma_R}$$

$b$ , the deviation from poisson distribution,  
is the strength of noise

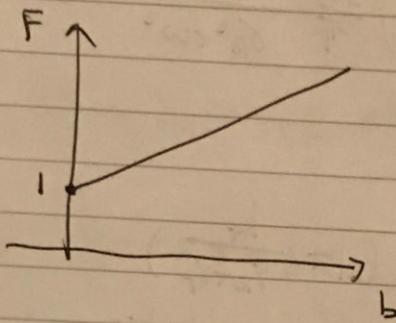
$\phi$  is the ratio between decay rates of RNA and protein. This ~~represents~~ represents the instability of protein production.

If possionian  $F = 1$

RNA much more unstable than protein

$$\therefore \phi \approx 0$$

$$F = 1 + b = \cancel{1+b}$$



~~more~~ higher production rate of protein,  
higher fluctuations in the protein ~~with~~  
concentration

- Intrinsic noise is caused by ~~the~~ stochastic fluctuations within a cell (translation or transcription)
- Extrinsic noise is caused by differences between cells (number of ribosomes or copy numbers of key proteins).
- beneficial : optimize growth rate of cells
- deleterious : more prone to virus infection.